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⑤④ Coated aluminum material

⑤⑦ A coated aluminum material comprising an aluminum material and an aqueous coating composition coated on the surface thereof, wherein the aqueous coating composition comprises (A) a water-soluble or water-dispersible synthetic resin, (B) a lubricant powder, (C) silica particles and (D) a silane coupling agent.

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The present invention relates to a coated aluminum material excellent in corrosion resistance, electrodeposition coating properties, press forming properties, chemical conversion treatment resistance, etc.

In recent years, light weight aluminum materials made of aluminum or an aluminum alloy have been used as exterior panels of e.g. automobile bodies, and automobile bodies constructed by a combination of steel materials and aluminum materials have been on the market. Such automobile bodies constructed by a combination of steel materials and aluminum materials are produced, for example, by assembling independently fabricated steel materials and aluminum materials, subjecting the assembly to degreasing and chemical conversion treatment and then sequentially and continuously applying electrodeposition coating, intermediate coating and top coating thereto.

However, conventional aluminum materials are poor in the press forming properties. Further, aluminum materials are hardly degreased as compared with steel materials when press oil or rust preventive oil used during the fabrication is to be removed. Accordingly, when chemical conversion treatment such as zinc phosphate treatment is applied thereto, irregularity in the chemical conversion treatment is likely to result on its surface, whereby the corrosion resistance, the water resistant secondary adhesion or the like tends to be poor, and elution of aluminum is likely to occur during the chemical conversion treatment, and if the amount of such elution exceeds a certain level, the chemical conversion treatment tends to be hindered. Further, as the aluminum materials are used in combination with steel materials, there has been a problem that galvanic corrosion of aluminum materials is likely to result due to the contact of different metals.

To improve the press forming properties in an attempt to overcome the above problem, there have been proposed, for example, a method of changing the metal composition in an aluminum alloy (Japanese Unexamined Patent Publications No. 171547/1983, No. 201748/1986, No. 201749/1986 and No. 27544/1987), and a method of roughening the surface of an aluminum material (Japanese Unexamined Patent Publications No. 276707/1986 and No. 21047/1989). However, these methods provide no solution to the above-mentioned problems with respect to the corrosion resistance, water resistant secondary adhesion and galvanic corrosion resistance.

Further, to prevent irregularity in chemical conversion treatment, there have been proposed, for example, a method of chemically cleaning the surface of an aluminum material (e.g. Japanese Unexamined Patent Publications No. 240675/1989, NO. 279788/1989 and No. 57692/1990), and a method of lowering the viscosity of the rust preventive oil to facilitate degreasing (e.g. Japanese Unexamined Patent Publication No. 115385/1990). In order to make the same chemical conversion treatment applicable to an aluminum material and a steel material, a method has been proposed in which the surface area ratio of the two materials has been specified (e.g. Japanese Unexamined Patent Publication No. 104089/1986). However, none of such methods solves the problem with respect to the press forming properties.

In the above method, it has also been proposed that the surface of the aluminum material is preliminarily treated by prime-coating and the coated aluminum material having a prime-coating applied thereto is fabricated and assembled with a steel material (e.g. Japanese Unexamined Patent Publications No. 180218/1991 and No. 9476/1992). However, such a method has problems that in the subsequent chemical conversion treatment, the coating film is likely to be peeled, whereby the corrosion resistance will deteriorate, that the electric deposition coating in the subsequent step tends to be poor, and that the press forming properties tend to be poor. Thus, a practically useful coating material which fully satisfies the requirements for e.g. the chemical conversion treatment resistance, the corrosion resistance, the press forming properties and the electric deposition coating properties, has not yet been developed. Under these circumstances, in order to solve such problems, the present inventors developed an organic solvent-type coating composition for aluminum materials, which comprises a lubricant powder and an epoxy resin composed of epichlorohydrin skeletons and bisphenol skeletons comprising bisphenol A skeleton and bisphenol F skeleton, and filed a patent application (Japanese Unexamined Patent Publication No. 277577/1992). The coated aluminum material having such a coating composition applied, has improved chemical conversion treatment resistance, corrosion resistance, press forming properties and electric deposition coating properties. However, at present, higher performance is required with respect to the corrosion resistance, the press forming properties, etc. than the performance required at the time of filing the application. Further, a demand for an aqueous coating material has increased from the viewpoint of environmental protection.

Under these circumstances, it is an object of the present invention to provide a coated aluminum material having formed on the surface of an aluminum material a coating film excellent in the chemical conversion treatment resistance, corrosion resistance, press forming properties, electric deposition coating properties, etc.

To fulfil the above object, the present invention provides a coated aluminum material comprising an aluminum material and an aqueous coating composition coated on the surface thereof, wherein the aqueous

coating composition comprises (A) a water-soluble or water-dispersible synthetic resin, (B) a lubricant powder, (C) silica particles and (D) a silane coupling agent.

Now, the present invention will be described in detail with reference to the preferred embodiments.

As the water-soluble or water-dispersible synthetic resin (A) constituting the coating composition to be used in the present invention, an epoxy resin, an acryl-modified epoxy resin or an anionic urethane resin is particularly preferred.

The epoxy resin may, for example, be ① an epoxy resin obtained by subjecting a bisphenol such as bisphenol A, bisphenol F or bisphenol AD, and epichlorohydrin to a condensation reaction by a conventional method, or the one obtained by reacting such a resin with a polyfunctional compound such as metaxylene diamine, hexamethylene diisocyanate or ethylene glycol and forming the resulting epoxy resin of a higher molecular weight containing at least two epoxy groups per molecule, into an aqueous dispersion in combination with a surfactant, or ② the one obtained by modifying such a resin with a basic nitrogen compound such as propylamine, butylamine or diethylamine or by a polybasic acid or its acid anhydride, such as isophthalic acid, succinic acid or phthalic anhydride, followed by neutralization to form an aqueous solution or aqueous dispersion. The molecular weight of the epoxy resin is usually from about 500 to 100,000, preferably from 500 to 10,000. If the molecular weight is smaller than this range, the coating film properties such as corrosion resistance, alkali resistance and water resistance tend to be low. On the other hand, if it is larger than the above range, it tends to be difficult to obtain an aqueous solution or an aqueous dispersion.

The above acryl-modified epoxy resin may, for example, be a resin which is produced as follows. Namely, a bisphenol type epoxy resin and a polymerizable unsaturated group-containing polybasic acid or its acid anhydride are heated and reacted in a solvent in the presence of a catalyst to introduce a polymerizable unsaturated group to the bisphenol type epoxy resin. Then, this bisphenol type epoxy resin having a polymerizable unsaturated group and a polymerizable unsaturated monomer component are heated and reacted for graft polymerization to obtain an acryl-modified epoxy resin.

As the above bisphenol type epoxy resin, a bisphenol A type epoxy resin, a bisphenol F type epoxy resin or a mixture thereof can be used, and the one having an epoxy equivalent of from 170 to 3,500, preferably from 800 to 2,500, is preferred.

Specific examples of the bisphenol type epoxy resin include commercial products such as Epikote 801, 802, 807, 815, 819, 825, 827, 828, 834, 1001, 1002, 1003, 1004, 1007 and 1010 (tradenames, manufactured by Yuka Shell Epoxy K.K.); DER317, 324, 325, 330, 331J, 337, 343, 361, 661 and 662 (tradenames, manufactured by Dow Chemical); Epichlon 840, 850, 855, 1,050 and 1055 (tradenames, manufactured by Dainippon Ink and Chemicals, Inc.); and Araldite GY250, 260, 280, 255, 257, 6071 and 7072 (tradenames, manufactured by Ciba Geigy).

The above-mentioned polymerizable unsaturated group-containing polybasic acid or its acid anhydride may, for example, be maleic acid, fumaric acid, itaconic acid, citraconic acid or acid anhydrides thereof, as typical examples.

As examples of the above polymerizable unsaturated monomer component, a carboxyl group-containing polymerizable unsaturated monomer such as (meth)acrylic acid, maleic acid, fumaric acid, itaconic acid or maleic anhydride, is used as an essential constituting monomer, and a hydroxyl group-containing monomer such as hydroxyethyl (meth)acrylate, hydropropyl (meth)acrylate or hydroxybutyl (meth)acrylate; an acetoacetyl group-containing monomer such as acetoacetoxyethyl (meth)acrylate; a (meth)acrylic acid ester monomer such as methyl (meth)acrylate, ethyl (meth)acrylate, propyl (meth)acrylate, butyl (meth)acrylate, 2-ethylhexyl (meth)acrylate, lauryl (meth)acrylate or cyclohexyl (meth)acrylate; styrene or a substituted styrene monomer such as vinyltoluene or methylstyrene; (meth)acrylonitrile, vinyl chloride, vinyl acetate, vinyl propionate, a maleic acid dialkyl ester, may be mentioned. These monomers may be used alone or in combination as a mixture of two or more of them.

The above-mentioned catalyst for reaction may, for example, be a tertiary amine such as triethylamine, a quaternary ammonium salt compound such as tetramethylammonium chloride, a lithium compound such as lithium chloride or lithium bromide, an imidazole compound such as butyl imidazole, sodium acetate, sodium phenolate, 1,8-diazabicyclo(5.4.0)-7-undecene, sodium hydroxide, or potassium hydroxide.

The reaction of the bisphenol type epoxy resin with a polymerizable unsaturated group-containing polybasic acid or its acid anhydride is carried out to introduce a polymerizable unsaturated group to the bisphenol type epoxy resin, so that a polymerizable unsaturated monomer component can be grafted, as described above. Therefore, the equivalent ratio of the epoxy groups of the bisphenol type epoxy resin to the carboxyl groups of the polymerizable unsaturated group-containing polybasic acid or its acid anhydride is usually from 1:0.05 to 1:0.8, preferably from 1:0.1 to 1:0.3. If the polybasic acid or its acid anhydride is less than the above range, the graft active sites for grafting the polymerizable unsaturated monomer

component tend to be less, whereby the effect for modifying the acrylic resin i.e. the solubility or the dispersion stability of the acryl-modified epoxy resin in water as the solvent, tends to be low, or the flexibility of the coating film thereby obtained tends to be poor. On the other hand, if it exceeds the above range, gelation is likely to occur during the graft polymerization.

5 By the reaction of the bisphenol type epoxy resin with the polymerizable unsaturated group-containing polybasic acid or its acid anhydride, the polymerizable unsaturated group is introduced, and to the polymerizable unsaturated group, the polymerizable unsaturated monomer component is grafted to obtain an acryl-modified epoxy resin. As the polymerizable unsaturated monomer component to be used here, a carboxyl group-containing polymerizable unsaturated monomer is used as an essential component.

10 The carboxyl group-containing polymerizable unsaturated monomer is used to introduce a carboxyl group to the resin so that the resulting acryl-modified epoxy resin can be dissolved or stably dispersed in water as the solvent, when it is neutralized by a neutralizing agent. Further, the carboxyl group will also contribute to improvement of the adhesion of the resulting coating film.

Accordingly, the amount of the carboxyl group-containing polymerizable unsaturated monomer to be used, is preferably such that the acid value of the resulting acryl-modified epoxy resin will be at least about 15 20, preferably from 40 to 200.

Further, in order to improve the adhesion of the coating film or the storage stability of the coating composition, it is preferred to use a hydroxyl group-containing monomer in combination with the polymerizable unsaturated monomer component, in such an amount that the hydroxyl value of the acryl- 20 modified epoxy resin will be from about 10 to 50. Likewise, in order to improve the adhesion, corrosion resistance, boiling water resistance and alkali resistance of the obtained coating film, it is advisable to incorporate an acetoacetyl group-containing polymerizable unsaturated monomer in an amount of from 1 to 20 wt% of the polymerizable unsaturated monomer component.

The acryl-modified epoxy resin usually has a weight average molecular weight of about 2,000 to 25 100,000, preferably from 4,000 to 70,000. The weight ratio of the bisphenol type epoxy resin to the polymerizable unsaturated monomer to be graft polymerized thereto, is preferably within a range of from 4:6 to 9:1.

If the polymerizable unsaturated monomer is less than the above range, the flexibility of the resulting coating film and the corrosion resistance of the press forming portion tend to be poor. On the other hand, if 30 it exceeds the above range, the bisphenol type epoxy resin decreases correspondingly, whereby the adhesion, corrosion resistance or the like of the resulting coating film tends to be low. The acryl-modified epoxy resin is neutralized by a neutralizing agent and used in such a state that it can be diluted with water so that it will be dissolved or stably dispersed in water. As such a neutralizing agent, ammonia, methylamine, dimethylamine, trimethylamine, ethylamine, diethylamine, triethylamine, 35 dimethylethanolamine, monoethanolamine, diethanolamine, triethanolamine or morpholine may be mentioned as typical examples.

The above anionic urethane resin is the one obtained by dissolving or stably dispersing in water a polyurethane resin which is in turn obtained by chain-extending a polyurethane made from a polyol such as polyester polyol or polyether polyol and an aromatic, aliphatic or alicyclic diisocyanate, with a low molecular 40 weight compound having at least two active hydrogen atoms such as a diol, a diamine or a dicarboxylic acid. As such a resin, conventional materials can widely be used.

The polyol useful for the synthesis of the anionic aqueous urethane resin to be used in the present invention, may, for example, be a polyhydroxy compound such as a polyether, a polyacetal, a polyester, a polyamide or a polyesteramide.

45 The polyether may, for example, be a polymer, copolymer or graft polymer of ethylene oxide, propylene oxide, tetrahydrofuran or butylene oxide, or a copolymer thereof, a polyether obtained by condensation of a polyhydric alcohol or a mixture of polyhydric alcohols, or a polyether obtained by alkoxylation of a polyhydric alcohol, an amine polyamine and an aminoalcohol. The polyacetal may, for example, be the one prepared from hexanediol and formaldehyde.

50 Further, as the polyester, the polyester amide and the polyamide, mainly linear condensation products obtainable from polybasic saturated and unsaturated carboxylic acids and polyhydric saturated and unsaturated alcohols, aminoalcohols, diamine polyamines and their mixtures, may be used.

Further, as the isocyanate, any aromatic or aliphatic diisocyanate may be employed. Examples of such diisocyanate include hexamethylene diisocyanate, tetramethylene diisocyanate, 3,3'-dimethoxy-4,4'- 55 biphenylene diisocyanate, p-xylylene diisocyanate, m-xylylene diisocyanate, 1,3-diisocyanate methylcyclohexanone, 1,4-diisocyanate methylcyclohexanone, 4,4'-diisocyanate cyclohexanone, 4,4'-diisocyanate cyclohexylmethane, isophorone diisocyanate, 2,4-tolylene diisocyanate, 2,6-tolylene diisocyanate, p-phenylene diisocyanate, diphenylmethane diisocyanate, m-phenylene diisocyanate, 2,4-naphthalene

diisocyanate, 3,3'-dimethyl-4,4'-biphenylene diisocyanate and 4,4'-diphenylene diisocyanate. Among these isocyanates, preferred are 2,4-tolylene diisocyanate, 2,6-tolylene diisocyanate, hexamethylene diisocyanate and isophorone diisocyanate.

Now, as the chain extender having at least two active hydrogens, useful for the synthesis of the anionic aqueous urethane resin to be used in the present invention, the following materials may be mentioned.

(1) A saturated or unsaturated glycol such as ethylene glycol or a condensation product of ethylene glycol, butanediol, propanediol, 1,3-propanediol, 1,2-neopentyl glycol, or a mono- or bis-alkoxylated aliphatic, alicyclic, aromatic or heterocyclic primary amine such as N-methyldiethanolamine, N-butyl-diethanolamine, N-oleyldiethanolamine or N-cyclohexyldiisopropanolamine.

(2) An aliphatic, alicyclic or aromatic diamine, such as ethylenediamine, hexamethylenediamine, 1,4-cyclohexyldiamine or an isomer of phenylenediamine.

(3) An amino alcohol such as ethanolamine, propanolamine or butanolamine.

(4) An aliphatic, alicyclic or aromatic dicarboxylic acid such as oxalic acid, malonic acid, adipic acid, pimelic acid, succinic acid, azelaic acid, sebacic acid, terephthalic acid, isophthalic acid or maleic acid.

The anionic urethane resin thus obtained, is neutralized by the above-mentioned neutralizing agent so that it is soluble or stably dispersed in water, and it is used in such a state that it can be diluted with water.

The lubricant powder (B) constituting the coating composition to be used in the present invention is preferably the one which maintains the powdery state at room temperature and after forming a coating film. Such a lubricant powder is incorporated to roughen the resulting coating film surface and thus to impart the lubricating properties i.e. to reduce the kinematic friction coefficient, thereby to improve the formability, particularly the press forming property, of the coated aluminum material. As such a lubricating powder, a synthetic wax powder and a solid lubricant powder may be mentioned as typical examples.

As the synthetic wax powder, a synthetic hydrocarbon; a fatty acid ester; a fatty acid nitrogen derivative such as a fatty acid amide or a substituted amide; a modified wax such as a montan wax derivative or oxidized montan wax; a high molecular weight compound such as polyester wax; and a chlorinated wax such as chlorinated paraffin, may, for example, be mentioned as typical examples. Particularly preferred is a synthetic wax powder having a saponification value and a high melting point.

As the solid lubricant powder, a laminar lubricant such as graphite, molybdenum disulfide, tungsten disulfide, boron nitride or fluorinated graphite; a plastic lubricant such as polyvinyl chloride, polystyrene, polymethyl (meth)acrylate, polyamide, high density polyethylene, polypropylene or polytetrafluoroethylene; a metal soap such as a calcium, barium, lithium, zinc or aluminum soap of a fatty acid, may, for example, be mentioned as typical examples. Particularly preferred is a plastic lubricant or a metal soap having a high surface lubricating property.

The lubricant powder usually has an average particle size of from 0.1 to 20  $\mu\text{m}$ . If the particle size is too small at a level of less than 0.1  $\mu\text{m}$ , the lubricant particles tend to be hardly exposed on the coating film, whereby the lubricating properties will be inadequate, and the press forming properties tend to be inferior. On the other hand, if the particle size is too large at a level exceeding 20  $\mu\text{m}$ , the film-forming property of the coating film and the stability of the coating material tend to have problems. A preferred range of the particle size of the lubricant powder is from 0.5 to 12  $\mu\text{m}$ .

The lubricant powder is incorporated preferably in an amount of from about 1 to 50 parts by weight, more preferably from 3 to 40 parts by weight, per 100 parts by weight of the water-soluble or water-dispersible synthetic resin (A), whereby the lubricating properties of the coating film will be obtained, and the physical properties and chemical strength of the coating film will be proper.

The silica particles (C) constituting the coating composition to be used in the present invention serve to roughen the coating film by their presence in the coating film and contribute to the corrosion resistance and press forming properties of the coated aluminum material as silanol groups present on the surface of the silica particles are bonded to the aluminum material. As such silica particles, water-dispersed uniform colloidal silica, water-dispersed aggregated colloidal silica and water-dispersible powdery fumed silica may be mentioned as typical examples.

Commercial products of water-dispersed uniform colloidal silica include, for example, Adelite AT-20N (tradename, manufactured Asahi Denka Kogyo K.K.), and Snowtex ST-Nup, Snowtex-up, Snowtex 20, Snowtex 30, Snowtex 40, Snowtex C, Snowtex N, Snowtex O, Snowtex S and Snowtex OL (tradenames, manufactured by Nissan Chemical Industries, Ltd.).

A commercial product of water-dispersed aggregated colloidal silica may, for example, be PT-3025 (tradename, Nissan Chemical Industries, Ltd.).

Commercial products of water-dispersible powdery fumed silica include, for example, Aerosil 130, Aerosil 200, Aerosil 300, Aerosil 380, Aerosil RX200, Aerosil R202, Aerosil T805, Aerosil R805, Aerosil OX50, Aerosil MOX80, Aerosil MOX170 and Aerosil COK84 (tradenames, manufactured by Nippon Aerosil

K.K.).

The silica particles are most preferably those having particle sizes within a range of from 0.01 to 2  $\mu\text{m}$  in a water-dispersed state, so that adequate effects for roughening the surface of the coating film can be obtained. If the particle size of silica particles is too small, the surface roughening of the coating film tends to be inadequate, and accordingly the press forming properties will be inferior. On the other hand, if the particle size exceeds 2  $\mu\text{m}$ , the film forming property (adhesion) of the coating film and the stability of the coating composition tend to be poor.

The silica particles are incorporated usually from about 5 to 100 parts by weight (as calculated as the solid content), preferably from 8 to 80 parts by weight, per 100 parts by weight of the water-soluble or water-dispersible synthetic resin (A). If the silica particles are less than this range, the surface roughening of the coating film tends to be inadequate, and if they are excessive, the film-forming property of the coating film and the stability of the coating composition tend to be poor.

The silane coupling agent (D) constituting the coating composition to be used in the present invention has a nature such that it is oriented to the surface of the aluminum material when coated. Accordingly, it forms a uniform barrier layer on the surface of the aluminum material and thus very much contributes to the improvement of corrosion resistance. Further, it is observed that the silane coupling agent reacts with the above-mentioned synthetic resin (A) and the silica particles (C) during the baking, and thus it very much contributes to the improvement of the adhesion of the coating film and to the fixing of silica particles.

The silane coupling agent may, for example, be  $\gamma$ -chloropropyltrimethoxysilane, vinyltrichlorosilane, vinyltriethoxysilane, vinyltrimethoxysilane, vinyl-tris( $\beta$ -methoxyethoxy)silane,  $\gamma$ -methacryloxypropyltrimethoxysilane,  $\beta$ -(3,4-epoxycyclohexyl)ethyltrimethoxysilane,  $\gamma$ -glycidoxypropyltrimethoxysilane,  $\gamma$ -mercaptopropyltrimethoxysilane,  $\gamma$ -aminopropyltriethoxysilane, N- $\beta$ -(aminoethyl)aminopropyltrimethoxysilane,  $\gamma$ -ureidopropyltriethoxysilane,  $\gamma$ -glycidoxypropylmethyldiethoxysilane,  $\gamma$ -glycidoxypropyldimethyl, or  $\gamma$ -glycidoxypropyldimethylethoxysilane.

The silane coupling agent is incorporated usually in an amount of from about 0.01 to 10 parts by weight (as calculated as a solid content), preferably from 0.05 to 8 parts by weight, per 100 parts by weight of the water-soluble or water-dispersible synthetic resin (A). If the silane coupling agent is less than this range, the above-mentioned effects tend to be hardly obtained. On the other hand, if it is excessive, the stability of the coating composition tends to be poor.

The coating composition to be used in the present invention is a coating material comprising the water-soluble or water-dispersible synthetic resin (A), the lubricant powder (B), the silica particles (C) and the silane coupling agent (D) described above, as essential constituting components and having such essential constituting components uniformly dispersed or dissolved in water to have a solid content of from about 10 to 40 wt%.

The coating composition to be used in the present invention may further contain a water-soluble organic solvent; a melamine resin, a benzoguanamine resin or a crosslinking agent such as a polyblocked isocyanate compound; an organic or inorganic pigment; an additive such as a dispersing agent, an antisetting agent or a levelling agent, or various modifying resins.

Now, method for producing a coated aluminum material of the present invention will be described.

As the aluminum material to be used in the present invention, those commonly used for press forming products, such as non-heat treated Al-Mg type 5000 type alloy, heat treated Al-Cu-Mg type 2000 type alloy, heat treated Al-Mg-Zn type 7000 type alloy, heat treated Al-Mg-Si type 6000 type alloy, non-heat treated Al-Mn type 3000 type alloy and 4000 type alloy, and non-heat treated pure aluminum type 1000 malleable material, may be mentioned as typical examples. However, the aluminum material is not limited to such specific examples.

The aluminum material may be an aluminum material having surface treatment applied by a conventional means, such as reactive chromate treatment with e.g. chromium chromate or phosphoric acid chromate, chromium treatment such as coating type chromate treatment or electrolytic chromate treatment, or non-chromium treatment such as zircon phosphate treatment, silane coupling treatment, titanium coupling treatment, zircon coupling treatment or aluminum coupling treatment.

The coated aluminum material of the present invention is prepared by coating the above described coating composition on the surface of such an aluminum material by such a means as spraying, roll coating or shower coating, followed by curing at a temperature of from 80 to 300 °C, preferably from 100 to 250 °C.

Even a thin film with a film thickness of about a few  $\mu\text{m}$  may provide an adequate performance, but the film thickness may be further increased. For example, the film thickness is preferably from 0.1 to 10  $\mu\text{m}$ , more preferably from 1 to 5  $\mu\text{m}$ .

The coated aluminum material thus obtained, is subjected to electric deposition coating or usual top coating and then applied in the fields of exterior panels of automobiles, household appliances and

construction materials.

By coating the above coating composition on the aluminum material, a coated aluminum material excellent in the corrosion resistance, the electric deposition coating property, the adhesion and the press forming properties, can be obtained. Especially when the coated aluminum material of the present invention is used as an aluminum material for the production of an automobile body by combined use of a steel material and the aluminum material, it provides excellent durability i.e. alkali resistant degreasing properties, against alkali treatment in the degreasing process, and in the subsequent chemical conversion treatment such as zinc phosphate treatment, a chemically converted coating film is formed only on the steel material, and no chemical coating film will be formed on the coated aluminum material. Accordingly, the coated aluminum material of the present invention is an aluminum material coated with a practically valuable coating material, which has various effects such that a defect of irregularities in the chemical conversion treatment which occurs on conventional aluminum materials, can be eliminated, the chemical conversion treatment resistance is good, the galvanic corrosion of the aluminum material due to contact of different metals between the steel material and the coated aluminum material can be prevented.

Now, the present invention will be described in further detail with reference to Examples. However, it should be understood that the present invention is by no means restricted by such specific Examples. In the Examples, "parts" and "%" mean "parts by weight" and "% by weight", respectively.

#### EXAMPLES 1 to 6 and COMPARATIVE EXAMPLES 1 to 4

A mixture comprising the epoxy resin aqueous solution (aqueous dispersion), the lubricant powder, the silica particles and the silane coupling agent as identified in Table 1 or 2, was diluted with deionized water to obtain a coating material having a solid content of 20%.

The obtained coating material was coated by roll coating on the surface treated aluminum material (thickness: 1.0 mm) as identified in Table 1 or 2 so that the dry film thickness would be 3  $\mu$ m and baked so that the maximum plate temperature became 150°C in 30 seconds, followed by tests on the corrosion resistance, the press forming properties, the alkali resistance, the chemical conversion treatment resistance, the electric deposition coating properties, the top coating adhesion, the water resistance, the lubricating properties and the stability of the coating material. The results are shown in Table 3.

As is apparent from Table 3, in Examples 1 to 6 in which the coating compositions of the present invention were used, the coating films had excellent properties. On the other hand, in Comparative Example 1 containing no lubricant powder, the press forming properties were inferior, in Comparative Example 2 containing no silica particles, the corrosion resistance was inferior, in Comparative Example 3 containing no silane coupling agent, the water resistance was inferior, and in Comparative Example 4 containing no silica particles and no silane coupling agent, the corrosion resistance was poor.

Table 1

		Examples					
		1	2	3	4	5	6
Aluminum alloy material (surface treatment)		5000 type alloy (coating type chromate treatment)	6000 type alloy (chromium chromate treatment)	2000 type alloy (non- treatment)	5000 type alloy (non- treatment)	2000 type alloy (silane coupling agent treatment)	6000 type alloy (non- treatment)
		a *1)	a *1)	b *2)	b *2)	c *3)	d *4)
Coating material compo- nents	Epoxy resin aqueous liquid	100	100	100	100	100	100
	Solid content (parts)						
	Lubricant powder	Fatty acid ester *5)	Poly- ethylene wax *6)	Tetra- fluoro- ethylene wax *7)	Calcium stearate *8)	Molybdenum disulfide *9)	Fatty acid ester *5)
Amount (parts)		15	3	8	40	25	32



Table 1 (continued)

	Examples					
	1	2	3	4	5	6
Coating material components	Silica particles	Water-dispersed aggregated colloidal silica *11)	Fumed silica *12)	Water-dispersed aggregated colloidal silica *11)	Same as the left	Water-dispersed uniform colloidal silica *10)
	Solid content (parts)	80	10	20	50	8
	Silane coupling agent	Epoxy-type silane coupling agent	Same as the left	Amine-type silane coupling agent	Same as the left	Mercaptan-type silane coupling agent
	Amount (parts)	8	2	5	0.05	0.08
						2

Table 2

	Comparative Examples			
	1	2	3	4
	5000 type alloy (coating type chromate treatment)	Same as the left	Same as the left	2000 type alloy (non-treatment)
Aluminum alloy material (surface treatment)	a *1)	a *1)	a *1)	b *2)
Epoxy resin aqueous liquid	100	100	100	100
Solid content (parts)	Nil	Fatty acid ester *5)	Same as the left	Tetra-fluoro-ethylene wax *7)
Lubricant powder	0	40	15	15
Amount (parts)				

Table 2 (continued)

		Comparative Examples			
		1	2	3	4
Coating material components	Silica particles	Water-dispersed uniform colloidal silica *10)	Nil	Water-dispersed uniform colloidal silica *10)	Nil
	Solid content (parts)	90	0	80	0
	Silane coupling agent	Epoxy-type silane coupling agent	Same as the left	Nil	Nil
	Amount (parts)	8	10	0	0

Table 3

	Examples						Comparative Examples			
	1	2	3	4	5	6	1	2	3	4
Coating film properties	Corrosion resistance *13)	⊙	⊙	⊙	⊙	⊙	Δ	X	Δ	X
	Press forming properties *14)	⊙	⊙	⊙	⊙	⊙	X	Δ	○	Δ
	Alkali resistance *15)	⊙	⊙	⊙	⊙	⊙	Δ	Δ	X	Δ
	Chemical conversion treatment resistance *16)	⊙	⊙	⊙	⊙	⊙	Δ	Δ	X	Δ
	Electric deposition coating properties *17)	⊙	⊙	⊙	⊙	⊙	○	X	○	X

Table 3 (continued)

	Examples						Comparative Examples			
	1	2	3	4	5	6	1	2	3	4
Coating film properties	⊙	⊙	⊙	⊙	⊙	⊙	○	×	△	×
Top coating adhesion *18)	⊙	⊙	⊙	⊙	⊙	⊙	○	×	△	×
Water resistance *19)	⊙	⊙	⊙	○	○	○	△	×	×	×
Lubricating properties *20)	⊙	⊙	⊙	⊙	⊙	⊙	×	△	○	△
Stability of coating material *21)	⊙	⊙	⊙	⊙	⊙	⊙	△	○	○	○

\*1) Aqueous dispersion of bisphenol A type epoxy resin,  
"Aquatoto 3540" (tradename, manufactured by Toto Kasei  
K.K.), epoxy equivalent: 1,800, molecular weight: about  
4,000, solid content: 55%

\*2) Aqueous solution of bisphenol A type amine-modified  
epoxy resin, "Adecaresin EPEC-0436" (tradename,  
manufactured by Asahi Denka Kogyo K.K.), epoxy  
equivalent: 0, molecular weight: about 4,000, solid  
content: 25%

\*3) Aqueous solution of anionic modified epoxy resin,  
"Adecaresin EPEA-0058" (tradename, manufactured by Asahi  
Denka Kogyo K.K.), epoxy equivalent: 250, molecular  
weight: about 500, solid content: 25%

\*4) Aqueous solution of acryl-modified bisphenol A type  
epoxy resin, "Hopesol GEA-060" (tradename, manufactured  
by Kyowa Hakko K.K.), epoxy equivalent: 0, solid content:  
25%

\*5) Average particle size: 10  $\mu\text{m}$

\*6) Average particle size: 1  $\mu\text{m}$

\*7) Average particle size: 5  $\mu\text{m}$

\*8) Average particle size: 3  $\mu\text{m}$

\*9) Average particle size: 1  $\mu\text{m}$

\*10) Average particle size: 0.01  $\mu\text{m}$

\*11) Average particle size: 0.5  $\mu\text{m}$

\*12) Average particle size: 0.2  $\mu\text{m}$

13\*) A cycle corrosion test was conducted whereby one  
cycle comprised steps of spraying a 5% sodium chloride

aqueous solution to a sample plate at 35°C for 4 hours,  
then drying the sample at 60°C for 2 hours and then  
leaving it in a relative humidity of 95% (moisture) at  
50°C for 2 hours, and the corrosion resistance was  
evaluated by the formation of white rust after 100  
cycles.

◎: No white rust formed

○: White rust of less than 5% (area ratio)

△: White rust of less than 15% (area ratio)

×: White rust exceeding 15% (area ratio)

\*14) A cycle corrosion test was conducted wherein one  
cycle comprised steps of drawing a sample plate punched  
out to have a diameter of 94 mm into a cylinder having a  
diameter of 50 mm and a depth of 25 mm (BHF=1 ton),  
spraying a 5% sodium chloride aqueous solution thereto at  
35°C for 4 hours after the drawing, then drying it at  
60°C for 2 hours and leaving it in a relative humidity of  
95% (moisture) at 50°C for 2 hours, and the press forming  
properties were evaluated by formation of white rust  
after 50 cycles.

◎: No white rust

○: White rust of less than 5% (area ratio)

△: White rust of less than 15% (area ratio)

×: White rust exceeding 15% (area ratio)

\*15) A sample plate was immersed in an alkali degreasing  
solution at 50°C for 5 minutes, then washed with water  
and dried. Then, cross cut lines were imparted thereto

by a cutter knife to form 100 cross cut squares of 1 mm<sup>2</sup>,  
and a peeling test was conducted by means of an adhesive  
tape, whereby the coating film remaining ratio was  
measured.

◎: Remaining ratio of 100%

○: Remaining ratio of from 95 to 99%

△: Remaining ratio of from 90 to 94%

×: Remaining ratio of less than 89%

\*16) A sample plate was immersed in a zinc phosphate  
treating solution at 45°C for 5 minutes, washed with  
water and dried, whereupon the coating film was  
inspected.

◎: No peeling of the coating film was observed, and  
the coating film was as uniform as prior to the  
chemical conversion treatment

○: Peeling of the coating film was slightly observed  
(less than 5%)

△: Peeling of the coating film was observed (at  
least 5%)

×: Peeling of the coating film was observed over the  
entire surface

\*17) An amine-added epoxy resin-block isocyanate type  
cation electric deposition coating material was cation  
electric deposition-coated on the surface of a sample  
plate at a bath temperature of 28°C at 100V for 3  
minutes, followed by baking at 165°C for 20 minutes,  
whereupon the appearance of the coating film (area: 100



cm<sup>2</sup>) was inspected.

- 5           ◎: Formation of gas pinholes and  
              craters           0
- :   Formation of gas pinholes and  
10               craters       1 to 5 points
- △:   Formation of gas pinholes and  
              craters       6 to 20 points
- 15           ×:   Formation of gas pinholes and  
              craters       more than 20 points

20   \*18) Cross cut lines were imparted to the cation electric  
deposition-coated plate obtained in \*17) by a cutter  
knife to form 100 cross cut squares of 1 mm<sup>2</sup>, and a  
25   peeling test was conducted by means of an adhesive tape,  
whereby the remaining ratio of the electric deposition  
coated film was measured.

- 30           ◎: 100%
- : 95 to 99%
- 35           △: 90 to 94%
- ×: 89% or less

40   \*19) The cation electric deposition coated plate obtained  
in \*17) was immersed in water at 40°C, then dried and  
subjected to the same peeling test as in \*18), whereby  
45   the remaining ratio of the electric deposition coated  
film was measured.

- ◎: Remaining ratio after immersion for 600 hours  
50               100%
- : Remaining ratio after immersion for 500 hours

55

100%

△: Remaining ratio after immersion for 500 hours

90 to 99%

×: Remaining ratio after immersion for 500 hours

89% or less

\*20) The lubricating properties were measured by means of a surface property measuring machine HEIDON-14 (manufactured by Shinto Kagaku K.K.) under a load of 50 g, with a ball indenter of 10 mm in diameter at a moving speed of 50 mm/min.

◎: Kinetic friction coefficient of less than 0.10

○: Kinetic friction coefficient of from 0.10 to less than 0.20

△: Kinetic friction coefficient of from 0.20 to less than 0.35

×: Kinetic friction coefficient of 0.35 or more

\*21) The coating material in each Example or Comparative Example was left to stand still at 50°C for 3 weeks and further at room temperature for one day, whereupon the condition of the coating material was inspected.

◎: Slight separation was observed, but re-dispersion was possible with stirring for 15 minutes.

○: Slight separation was observed, but re-dispersion was possible with stirring for 30 minutes.

△: Substantial separation was observed, but re-dispersion was possible with stirring for 30 minutes.

X: Substantial separation was observed, and re-  
dispersion was impossible with stirring for 30  
minutes.

Now, Examples will be given in which an acryl-modified epoxy resin was used as the synthetic resin.

10 Preparation of polymerizable unsaturated group-containing epoxy resin solution (A)

Into a reactor equipped with a stirrer, a reflux condenser, a nitrogen gas supply means and a thermometer, 696 parts of a bisphenol A type epoxy resin (Epikote 1007, tradename, manufactured by Yuka Shell Epoxy K.K., epoxy equivalent: 1,750 to 2,200) and 350 parts of ethylene glycol monobutyl ether were charged and dissolved under heating. Then, while introducing a nitrogen gas, 2 parts of fumaric acid and 0.1 part of triethylamine were added thereto with stirring, and the mixture was reacted at 130°C for 5 hours to obtain a polymerizable unsaturated group-containing epoxy resin solution (A) having a solid content of 67%. Here, the reaction was conducted under such a condition that the equivalent ratio of the epoxy groups of the above epoxy resin to the carboxyl groups of the polybasic acid was 1:0.1.

20 Preparation of polymerizable unsaturated group-containing epoxy resin solution (B)

A polymerizable unsaturated group-containing epoxy resin solution (B) having a solid content of 67% was obtained in the same manner as in the preparation of the above resin solution (A) except that the amount of fumaric acid was changed to 4 parts. The reaction was conducted under such a condition that the equivalent ratio of the epoxy groups of the epoxy resin to the carboxyl groups of the polybasic acid was 1:0.2.

30 Preparation of polymerizable unsaturated group-containing epoxy resin solution (C)

A polymerizable unsaturated group-containing epoxy resin solution (C) having a solid content of 67% was obtained in the same manner as in the preparation of the above resin solution (A) except that the amount of fumaric acid was changed to 6 parts. The reaction was conducted under such a condition that the equivalent ratio of the epoxy groups of the epoxy resin to the carboxyl groups of the polybasic acid was 1:0.3.

Preparation of acryl-modified epoxy resin aqueous solution (1)

40 Into the above-mentioned reactor, 105 parts of the polymerizable unsaturated group-containing epoxy resin solution (B) was charged and heated to 90°C. Then, a mixture comprising 16.2 parts of styrene, 8 parts of butyl acrylate, 5.8 parts of acrylic acid, 2.4 parts of azobisisobutyronitrile and 20 parts of ethylene glycol monobutyl ether, was dropwise added thereto with stirring over a period of 2 hours, and the mixture was further reacted at the same temperature for 4 hours. The mixture was cooled to 50°C, and a mixture comprising 5.7 parts of dimethylethanolamine and 170 parts of deionized water, was dropwise added thereto with stirring over a period of 30 minutes, to obtain an acryl-modified epoxy resin (acid value: 45, molecular weight: 42,000, epoxy resin/acryl monomer = 7/3) aqueous solution (1) having a solid content of 30%.

50 Preparation of acryl-modified epoxy resin aqueous solution (2)

An acryl-modified epoxy resin (acid value: 45, molecular weight: 52,000, epoxy resin/acryl monomer = 7/3) aqueous solution (2) having a solid content of 30%, was obtained in the same manner as in the preparation of the acryl-modified epoxy resin aqueous solution (1) except that the polymerizable unsaturated monomer components were changed to 12.8 parts of styrene, 6.4 parts of butyl acrylate, 5.8 parts of acrylic acid and 5 parts of acetoacetoxy methacrylate.

Preparation of acryl-modified epoxy resin aqueous solution (3)

An acryl-modified epoxy resin (acid value: 45, molecular weight: 50,000, epoxy resin/acryl monomer = 7/3) aqueous solution (3) having a solid content of 30%, was obtained in the same manner as in the preparation of the acryl-modified epoxy resin aqueous solution (1) except that the polymerizable unsaturated monomer components were changed to 8.8 parts of styrene, 6.4 parts of butyl acrylate, 5.8 parts of acrylic acid, 4 parts of 2-hydroxyethyl methacrylate and 5 parts of acetoacetoxy methacrylate.

Preparation of acryl-modified epoxy resin aqueous solution (4)

An acryl-modified epoxy resin (acid value: 45, molecular weight: 45,000, epoxy resin/acryl monomer = 7/3) aqueous solution (4) having a solid content of 30%, was obtained in the same manner as in the preparation of the acryl-modified epoxy resin aqueous solution (1) except that the polymerizable unsaturated monomer components were changed to 8.8 parts of styrene, 6.4 parts of butyl acrylate, 5.8 parts of acrylic acid, 4.0 parts of 2-hydroxyethyl methacrylate and 5 parts of methyl methacrylate.

Preparation of acryl-modified epoxy resin aqueous solution (5)

An acryl-modified epoxy resin (acid value: 45, molecular weight: 40,000, epoxy resin/acryl monomer = 7/3) aqueous solution (5) having a solid content of 30%, was obtained in the same manner as in the preparation of the acryl-modified epoxy resin aqueous solution (1) except that the polymerizable unsaturated group-containing epoxy resin solution was changed to (A), and the polymerizable unsaturated monomer components were changed to 12.8 parts of styrene, 6.4 parts of butyl acrylate, 5.8 parts of acrylic acid and 5 parts of acetoacetoxy methacrylate.

Preparation of acryl-modified epoxy resin aqueous solution (6)

An acryl-modified epoxy resin (acid value: 45, molecular weight: 45,000, epoxy resin/acryl monomer = 5/5) aqueous solution (6) having a solid content of 30%, was obtained in the same manner as in the preparation of the acryl-modified epoxy resin aqueous solution (1) except that the polymerizable unsaturated group-containing epoxy resin solution was changed to 75 parts of (C) and the polymerizable unsaturated monomer components were changed to 25 parts of styrene, 10.2 parts of butyl acrylate, 5.8 parts of acrylic acid, 4.0 parts of 2-hydroxyethyl methacrylate and 5 parts of acetoacetoxy methacrylate.

## EXAMPLES 7 to 12 and COMPARATIVE EXAMPLES 5 to 8

A mixture comprising the acryl-modified epoxy resin aqueous solution, the lubricant powder, the silica particles and the silane coupling agent as identified in Table 4 or 5, was diluted with deionized water to obtain a coating material having a solid content of 20%. The obtained coating material was coated on the surface treated aluminum material (thickness: 1.0 mm) as identified in Table 4 or 5 so that the dry film thickness would be 3  $\mu$ m and baked so that the maximum plate temperature reached became 150 °C in 30 seconds, followed by tests on the corrosion resistance, the press forming properties, the alkali resistance, the chemical conversion treatment resistance, the electric deposition coating properties, the top coating adhesion, the water resistance, the lubrication properties and the stability of the coating material. The results are shown in Table 6.

As is evident from Table 6, in Example 7 to 12 wherein the coating compositions of the present invention were used, the coating films had excellent properties. On the other hand, in Comparative Example 5 containing no lubricant powder, the press forming properties were inferior, in Comparative Example 6 containing no silica particles, the corrosion resistance was inferior, in Comparative Example 7 containing no silane coupling agent, the water resistance was inferior, and in Comparative Example 8 containing no silica particles and no silane coupling agent, the corrosion resistance was inferior.

Table 4

	Examples					
	7	8	9	10	11	12
Aluminum alloy material (surface treatment)	5000 type alloy (coating type chromate treatment)	6000 type alloy (chromium chromate treatment)	2000 type alloy (non-treatment)	5000 type alloy (non-treatment)	2000 type alloy (silane coupling agent treatment)	6000 type alloy (non-treatment)
Coating material components	Acryl-modified epoxy resin aqueous solution	(1)	(2)	(3)	(4)	(5)
	Solid content (parts)	100	100	100	100	100
	Lubricant powder	Fatty acid ester *5)	Poly-ethylene wax *6)	Tetra-fluoro-ethylene wax *7)	Calcium stearate *8)	Molybdenum disulfide *9)
	Amount (parts)	15	3	8	40	25
						32

Table 4 (continued)

Examples							
	7	8	9	10	11	12	
Coating material components	Silica particles	Water-dispersed uniform colloidal silica *10)	Water-dispersed aggregated colloidal silica *11)	Fumed silica *12)	Water-dispersed aggregated colloidal silica *11)	Same as the left	Water-dispersed uniform colloidal silica *10)
	Solid content (parts)	80	10	20	50	8	30
	Silane coupling agent	Epoxy-type silane coupling agent	Same as the left	Amine-type silane coupling agent	Same as the left	Mercaptan-type silane coupling agent	Same as the left
	Amount (parts)	8	2	5	0.05	0.08	2

Table 5

	Comparative Examples			
	5	6	7	8
Aluminum alloy material (surface treatment)	5000 type alloy (coating type chromate treatment)	Same as the left	Same as the left	2000 type alloy (non-treatment)
Coating material components	Acryl-modified epoxy resin aqueous solution	(1)	(2)	(3)
	Solid content (parts)	100	100	100
	Lubricant powder	Nil	Fatty acid ester #5)	Tetra-fluoro-ethylene wax #7)
	Amount (parts)	0	40	15

Table 5 (continued)

	Comparative Examples			
	5	6	7	8
Coating material components	Silica particles	Water-dispersed uniform colloidal silica *10)	Nil	Water-dispersed uniform colloidal silica *10)
	Solid content (parts)	90	0	80
	Silane coupling agent	Epoxy-type silane coupling agent	Same as the left	Nil
	Amount (parts)	8	10	0



Table 6

	Examples						Comparative Examples			
	7	8	9	10	11	12	5	6	7	8
Coating film properties	Corrosion resistance *13)	⊙	⊙	⊙	⊙	⊙	Δ	X	Δ	X
	Press forming properties *14)	⊙	⊙	⊙	⊙	⊙	X	Δ	○	Δ
	Alkali resistance *15)	⊙	⊙	⊙	⊙	⊙	Δ	Δ	X	Δ
	Chemical conversion treatment resistance *16)	⊙	⊙	⊙	⊙	⊙	Δ	Δ	X	Δ
	Electric deposition coating properties *17)	⊙	⊙	⊙	⊙	⊙	○	X	○	X

Table 6 (continued)

	Examples						Comparative Examples			
	7	8	9	10	11	12	5	6	7	8
Coating film properties	⊙	⊙	⊙	⊙	⊙	⊙	○	×	△	×
Top coating adhesion *18)	⊙	⊙	⊙	⊙	⊙	⊙	○	×	△	×
Water resistance *19)	⊙	⊙	⊙	○	○	○	△	×	×	×
Lubricating properties *20)	⊙	⊙	⊙	⊙	⊙	⊙	×	△	○	△
Stability of coating material *21)	⊙	⊙	⊙	⊙	⊙	⊙	△	○	○	○

Now, Examples in which an anionic urethane resin was used as the synthetic resin, will be described.

Preparation of anionic aqueous urethane resin solution (I)

Into a three-necked flask equipped with a reflux condenser, a thermometer and a stirrer, 292.1 parts of phthalic anhydride, 252.8 parts of adipic acid, 95.5 parts of trimellitic anhydride, 241.6 parts of ethylene glycol, 118.0 parts of trimethylol propane and 30.0 parts of xylene were added and heated to 220 °C over a period of 4 hours, and a condensation reaction was carried out. The reaction was terminated when the acid value became 40, and the reaction mixture was diluted with 866.0 parts of methyl ethyl ketone to obtain a polyester polyol resin having a solid content of 50%. Further, 1,000 parts of this polyester polyol resin was charged into a three-necked flask equipped with a reflux condenser, a thermometer and a stirrer, and while maintaining the temperature at 70 °C, 58.0 parts of hexamethylene diisocyanate was dropwise added thereto over a period of one hour. After completion of the dropwise addition, 36.0 parts of triethylamine was added thereto, and the mixture was further diluted with 900 parts of water. Then, the mixture was subjected to distillation under reduced pressure to recover methyl ethyl ketone and obtain an anionic urethane resin solution (I) having a solid content of 50% (weight average molecular weight: 25,000).

Preparation of anionic urethane resin solution (II)

Into the above three-necked flask, 700 parts of polyethylene glycol having a weight average molecular weight of 1,000, 14 parts of dimethylol propionic acid, 540 parts of methyl ethyl ketone and 320 parts of N-methylpyrrolidone were charged, and while maintaining the temperature at 70 °C, 86 parts of hexamethylene diisocyanate was dropwise added thereto over a period of one hour. Then, 10 parts of triethylamine was added thereto, and 600 parts of deionized water was further added thereto. Then, methyl ethyl ketone was distilled off by distillation under reduced pressure to obtain an anionic urethane resin (II) having a solid content of 50%, a number average molecular weight of 45,000 and an acid value of 70.

## EXAMPLES 13 to 18 and COMPARATIVE EXAMPLES 9 to 12

A mixture comprising the urethane resin aqueous solution (aqueous dispersion), the lubricant powder, the silane particles and the silane coupling agent, as identified in Table 7 or 8, was diluted with deionized water to obtain a coating material having a solid content of 20%.

The obtained coating material was roll-coated on the surface treated aluminum material (thickness: 1.0 mm) as identified in Table 7 or 8 so that the dry film thickness would be 3  $\mu$ m and baked so that the maximum temperature of the aluminum material became 150 °C in 30 seconds. This coated aluminum material was subjected to tests on the corrosion resistance, the press forming properties, the alkali resistance, the chemical conversion treatment resistance, the electric deposition coating properties, the top coating adhesion, the water resistance, the lubrication properties and the stability of the coating material. The results are shown in Table 9.

As is apparent from Table 9, the coating compositions of the present invention obtained in Examples 13 to 18 provided excellent coating film properties. On the other hand, in Comparative Example 9 containing no lubricant powder, the press forming properties were inferior, in Comparative Example 10 containing no silica particles, the corrosion resistance was inferior, in Comparative Example 11 containing no silane coupling agent, water resistance was inferior, and in Comparative Example 12 containing no silica particles and no silane coupling agent, corrosion resistance was inferior.

Table 7

	Examples					
	13	14	15	16	17	18
Aluminum alloy material (surface treatment)	5000 type alloy (coating type chromate treatment)	6000 type alloy (chromium chromate treatment)	2000 type alloy (non-treatment)	5000 type alloy (non-treatment)	2000 type alloy (silane coupling agent treatment)	6000 type alloy (non-treatment)
Coating material components	Aqueous urethane resin solution	(I)	(II)	(II)	(III) *22)	(IV) *23)
	Solid content (parts)	100	100	100	100	100
	Lubricant powder	Fatty acid ester *5)	Poly-ethylene wax *6)	Tetra-fluoro-ethylene wax *7)	Calcium stearate *8)	Molybdenum disulfide *9)
	Amount (parts)	15	3	8	40	25
						32

\*22) Superflex 110, manufactured by Daiichi Kogyo Seiyaku K.K.

\*23) Adecabontiter HUX-232, manufactured by Asahi Denka Kogyo K.K.

Table 7 (continued)

Examples							
	13	14	15	16	17	18	
Coating material components	Silica particles	Water-dispersed uniform colloidal silica *10)	Water-dispersed aggregated colloidal silica *11)	Pumed silica *12)	Water-dispersed aggregated colloidal silica *11)	Same as the left	Water-dispersed uniform colloidal silica *10)
	Solid content (parts)	80	10	20	50	8	30
	Silane coupling agent	Epoxy-type silane coupling agent	Same as the left	Amine-type silane coupling agent	Same as the left	Mercaptan-type silane coupling agent	Same as the left
	Amount (parts)	8	2	5	0.05	0.08	2

Table 8

	Comparative Examples			
	9	10	11	12
Aluminum alloy material (surface treatment)	5000 type alloy (coating type chromate treatment)	Same as the left	Same as the left	2000 type alloy (non-treatment)
Coating material components	Aqueous urethane resin solution	(I)	(II)	(II)
	Solid content (parts)	100	100	100
	Lubricant powder	Nil	Fatty acid ester *5)	Tetra-fluoro-ethylene wax *7)
	Amount (parts)	0	40	15

Table 8 (continued)

		Comparative Examples			
		9	10	11	12
Coating material components	Silica particles	Water-dispersed uniform colloidal silica *10)	Nil	Water-dispersed uniform colloidal silica *10)	Nil
	Solid content (parts)	90	0	80	0
	Silane coupling agent	Epoxy-type silane coupling agent	Same as the left	Nil	Nil
	Amount (parts)	8	10	0	0

Table 9

	Examples						Comparative Examples			
	13	14	15	16	17	18	9	10	11	12
Coating film properties	Corrosion resistance *13)	⊙	⊙	⊙	⊙	⊙	△	×	△	×
	Press forming properties *14)	⊙	⊙	⊙	⊙	⊙	×	△	○	△
	Alkali resistance *15)	⊙	⊙	⊙	⊙	⊙	△	△	×	△
	Chemical conversion treatment resistance *16)	⊙	⊙	⊙	⊙	⊙	△	△	×	△
	Electric deposition coating properties *17)	⊙	⊙	⊙	⊙	⊙	○	×	○	×



Table 9 (continued)

	Examples						Comparative Examples			
	13	14	15	16	17	18	9	10	11	12
Coating film properties	⊙	⊙	⊙	⊙	⊙	⊙	○	×	△	×
Top coating adhesion *18)	⊙	⊙	⊙	⊙	⊙	⊙	○	×	△	×
Water resistance *19)	⊙	⊙	⊙	○	○	○	△	×	×	×
Lubricating properties *20)	⊙	⊙	⊙	⊙	⊙	⊙	×	△	○	△
Stability of coating material *21)	⊙	⊙	⊙	⊙	⊙	⊙	△	○	○	○

## 55 Claims

1. A coated aluminum material comprising an aluminum material and an aqueous coating composition coated on the surface thereof, wherein the aqueous coating composition comprises (A) a water-soluble

or water-dispersible synthetic resin, (B) a lubricant powder, (C) silica particles and (D) a silane coupling agent.

- 5     2. The coated aluminum material according to Claim 1, wherein the aqueous coating composition is a composition comprising 100 parts by weight of (A) a water-soluble or water-dispersible synthetic resin, from 1 to 50 parts by weight of (B) a lubricant powder, from 5 to 100 parts by weight of (C) silica particles and from 0.01 to 10 parts by weight of (D) a silane coupling agent, and having a solid content of from 10 to 40 wt%.
- 10    3. The coated aluminum material according to Claim 1 or 2, wherein the water-soluble or water-dispersible synthetic resin (A) is an epoxy resin.
- 15    4. The coated aluminum material according to Claim 1 or 2, wherein the water-soluble or water-dispersible synthetic resin (A) is an acryl-modified epoxy resin obtained by graft polymerizing a polymerizable unsaturated monomer component containing a carboxyl group-containing polymerizable unsaturated monomer to a bisphenol type epoxy resin by means of a polymerizable unsaturated group-containing polybasic acid or its acid anhydride.
- 20    5. The coated aluminum material according to Claim 4, wherein the polymerizable unsaturated monomer component contains an acetoacetyl group-containing polymerizable unsaturated monomer.
- 25    6. The coated aluminum material according to Claim 4 or 5, wherein the acryl-modified epoxy resin has a weight ratio of the bisphenol type epoxy resin to the polymerizable unsaturated monomer component graft-polymerized to the epoxy resin of from 4:6 to 9:1.
- 30    7. The coated aluminum material according to Claim 1 or 2, wherein the water-soluble or water-dispersible synthetic resin (A) is an anionic urethane resin.
- 35    8. The coated aluminum material according to any one of Claims 1 to 7, which is for an exterior panel of an automobile body.

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